

# Polyaniline/Fe<sub>3</sub>O<sub>4</sub>/Poly (Methyl Methacrylate) Nanocomposites as an Acrylic Resin Coating for Enhancement of Anticorrosion Properties of Alkyd Paints

Hamidreza Ghafouri Taleghani<sup>1</sup>, Mohammad Soleimani-Lashkenari<sup>2,\*</sup>, Shiva Fazli<sup>3</sup> and Mohsen Ghorbani<sup>4</sup>

<sup>1</sup>Department of Chemical Engineering, University of Mazandaran, Babolsar, Iran

<sup>2</sup>Fuel Cell Electrochemistry and Advanced Material Research Laboratory, Faculty of Engineering Modern Technologies, Amol University of Special Modern Technologies, Amol, Iran

<sup>3</sup>Department of Chemical Engineering, Mazandaran University of Science & Technology, Babol, Iran

<sup>4</sup>Department of Chemical Engineering, Babol Noshirvani University of Technology, Babol, Iran

(\*) Corresponding author: m.soleimani@ausmt.ac.ir

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## Abstract

The exceptional application of nanocomposites containing polyaniline as a conductive polymer, poly(methyl methacrylate) (PMMA) as an acrylic resin and Fe<sub>3</sub>O<sub>4</sub> nanoparticles, for corrosion protection of mild steel was reported. The synthesized nanocomposites, were characterized with different techniques. The resulting PMMA/Polyaniline/Fe<sub>3</sub>O<sub>4</sub> nanocomposites were mixed with industrial alkyd paint to be employed as an anti-corrosion layer for mild steel in a NaCl solution. Accordingly, the potentiodynamic polarization and electrochemical impedance spectroscopy (EIS) were applied in order to investigate the corrosion behavior of the coated mild steel. Based on the results, the nanocomposites showed outstanding anti-corrosion properties compared with other composites coating. After investigating various compositions of the nanocomposites (3, 6, 9 and 12%) in the alkyd paint, the ideal composition related to the most favorable corrosion protection was obtained for the paint mixture comprising 6% nanocomposites.

**Keywords:** Polyaniline, Fe<sub>3</sub>O<sub>4</sub> nanoparticles, PMMA, Anti-corrosion, Electrochemical impedance.

## 1. INTRODUCTION

One of the most important issues that industries face is the lack of safety in equipment as well as high level of environmental pollutants released by material damages, caused by corrosion [1]. According to the study reported by National Association of Corrosion Engineers (NACE) International, "International Measures of Prevention, Application, and Economics of Corrosion Technology (IMPACT)", it was estimated that the total annual cost caused by corrosion in the world is about \$2.5 trillion [2]. The most important contributing factors in material

corrosion and coating damage are the nature of the aqueous environment in which materials are operating or placed [3]. When it comes to acidic media, the situation would be worse. There is no possibility to entirely prevent material from corrosion; however, new methodologies with special coating, protective metals, and corrosion inhibitors have been suggested to impede the corrosion processes, or improving the longevity of materials [4].

Among various metals, mild steel has been focused on by many researchers due to their excellent mechanical properties, that

are reasonable for many applications such as fatigue strength, fracture toughness, as well as their relatively low price [5]. Nevertheless, the poor durability of mild steel against corrosion is often problematic [6]. According to previous research works, one way to promote corrosion behavior of metals is employing coating [7]. Nowadays, the natural strength and reasonable price of polymers as an anti-corrosion coating make them valuable choices in research experiments [8]. As among, conducting polymers, such as polyaniline (PANI), are highly dispersed in a classical polymer binder and can provide numerous advantages including protecting metals against corrosion [9]. A study revealed that PANI, as a conductive polymer, and poly methyl methacrylate (PMMA) with hydrophobic properties help to prepare high active surface polymers [10]. The corrosion inhibition can be controlled through the use of PANI/PMMA polymers owing to their outstanding features such as hydrophobic nature, low poisonous behavior and facile single-step synthesis. However, polymer-based coating has poor adhesion and low thermal stability to metal surfaces, while inorganic materials, namely nanoparticles, can significantly overcome these problems [11]. Therefore, organic-mineral nanocomposite coating is associated with high mechanical and anti-corrosion properties in organic and inorganic networks [12].

In recent decades, nanotechnology and their applications were highly concentrated on by coating industries, where conventional additives and pigments are being explored to be replaced by nanoparticles in the composite coating [13]. For instance, in a research reported by Javidparvar et al. [14],  $\text{Fe}_3\text{O}_4$  nanopigments were synthesized through a hydrothermal method. Their results showed that the surface modification of the nanoparticles had a significant effect on epoxy coating resistance against corrosion. In another study, Mammeri et al. [15] indicated that employing PMMA- $\text{SiO}_2$  coating, which

were fabricated through a sol-gel method, resulted in desirable elastic modulus and hardness values. Moreover, an increase in  $\text{SiO}_2$  content in the coating was responsible for more desirable elastic properties. In another research work, Ni-P and Ni-P- $\text{Al}_2\text{O}_3$  electroless coatings were deposited on the surface of AISI 1045 steel discs. This study suggested that the presence of Al particles in Ni-P coating network resulted in an improvement in the wear resistance and hardness of the deposits. Furthermore, the coating treated at 400 °C possessed the greatest hardness as well as wear resistance. In a research work conducted by Alirezai et al. [16], the influence of two surfactants, namely sodium dodecyl sulphate (SDS) and dodecyl trimethyl ammonium bromide (DTAB), on the corrosion behavior of a low carbon steel substrate coated with Ni-P- $\text{TiO}_2$  nanoparticles was investigated. According to this study, a uniform distribution of  $\text{TiO}_2$  nanoparticles was achieved at an optimum concentration of DTAB. Besides, an improved corrosion behavior was obtained when the nanoparticles were incorporated in the Ni-P matrix. They claimed that, as a result, Ni-P- $\text{TiO}_2$  coating corrosion resistant was strongly related to the type and concentration of surfactant used. According to previous works, the control of nanoparticles size and their positioning in optimal regions is the primary purpose of fabricating nanocomposites that are intrinsically prone to create substantial aggregates [17]. Hence, using surfactants and polymers, both serving as capping agents, has been recommended.

In preliminary studies a new design of different coating with various concentrations of nanopaints in a pure form or in combination with industrial paints was widely used to protect mild steel from corrosion in saline environments, and also from the diffusion of water vapor, oxygen, and ions [18].

In this study, due to the in-situ emulsion polymerization synthesis, environmental compatibility, and low-temperature coating

preparation of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites, these nanocomposites were investigated as a promising organic-inorganic additive. Furthermore, structural, thermal and mechanical properties of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating was evaluated. Firstly, Fourier transform infrared spectroscopy (FTIR), X-ray diffraction (XRD), scanning and transmission electron microscopy (SEM & TEM), and thermal gravimetric analysis (TGA) were employed so as to characterize the morphologies of the nanocomposite coating. Eventually, the corrosion resistance property of a different nanocomposite coating over mild steel was evaluated using electrochemical methods such as Tafel polarization and electrochemical impedance spectroscopy (EIS) in a standard saline solution.

## 2. MATERIALS AND METHODS

### 2.1. Materials

All materials used in this work were purchased from Merck, Germany. Also, aniline monomer was distilled and stored at low temperature prior to experiments. The schematic illustration of the formation and modification of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating is provided in Figure 1. It should be stated that, during experiments, all agents were used without further purification. Moreover, all the solutions were prepared with deionized water (DIW, 18.2 MΩ).

### 2.2. Synthesis of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> Nanocomposite Coating

#### 2.2.1. Preparation of Fe<sub>3</sub>O<sub>4</sub> Nanoparticles

Fe<sub>3</sub>O<sub>4</sub> nanoparticles with a large number of exposed Fe-O groups were synthesized by a co-precipitation method. To do so, at first, a mixture containing 20 g of FeSO<sub>4</sub>.7H<sub>2</sub>O and 40 g of FeCl<sub>3</sub>.6H<sub>2</sub>O in 300ml distilled water under continuous stirring to form a colloidal solution. Then, 30 ml of NH<sub>3</sub> solution was dissolved in 170 ml deionized water and the temperature was fixed at 70°C. This solution, afterward, was

drop wise added to the colloid solution, which was stirring at 70°C. The reagents had been being boiled and refluxed for 30 min, under stirring condition. Eventually, the resulting dark emulsion was separated, washed by distilled water three times, and dried at 50°C for 24 h under vacuum condition [19, 20].

#### 2.2.2. Preparation of PANI/ Fe<sub>3</sub>O<sub>4</sub> Nanocomposites

PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites were prepared by chemical emulsion polymerization. In this method, initially, 0.2 g of HPC was dissolved in 100 ml aqueous solution (1M H<sub>2</sub>SO<sub>4</sub>). Then, 1 g of KIO<sub>3</sub> as an oxidant and 1 g of Fe<sub>3</sub>O<sub>4</sub> nanoparticles were added to stirred above aqueous solution. It took almost 30 min to completely disperse the mixture. Finally, 1 ml of freshly aniline monomer was gradually added into the resulting mixture at 800 rpm for about 6 hours. The extraction of the PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites was conducted through centrifuging at 6000 rpm for 5 min, washing with deionized water to remove the excess acid, and storing under vacuum condition at 60°C for 24 h. PANI in a conducting form, emeraldine salt (ES), was successfully obtained after observing a dark green color of all four samples [21, 22].

#### 2.2.3. Synthesis of PMMA

PMMA as a resin was synthesized using the following procedure: 3 g of C<sub>14</sub>H<sub>10</sub>O<sub>4</sub> particles had been being dispersed in 20 ml MMA under sonication for 30 min until the total dissolution of C<sub>14</sub>H<sub>10</sub>O<sub>4</sub> particles was achieved. At the end, the solution was stirred at 400 rpm for 24 h.

#### 2.2.4. Synthesis of PMMA/ PANI/Fe<sub>3</sub>O<sub>4</sub>

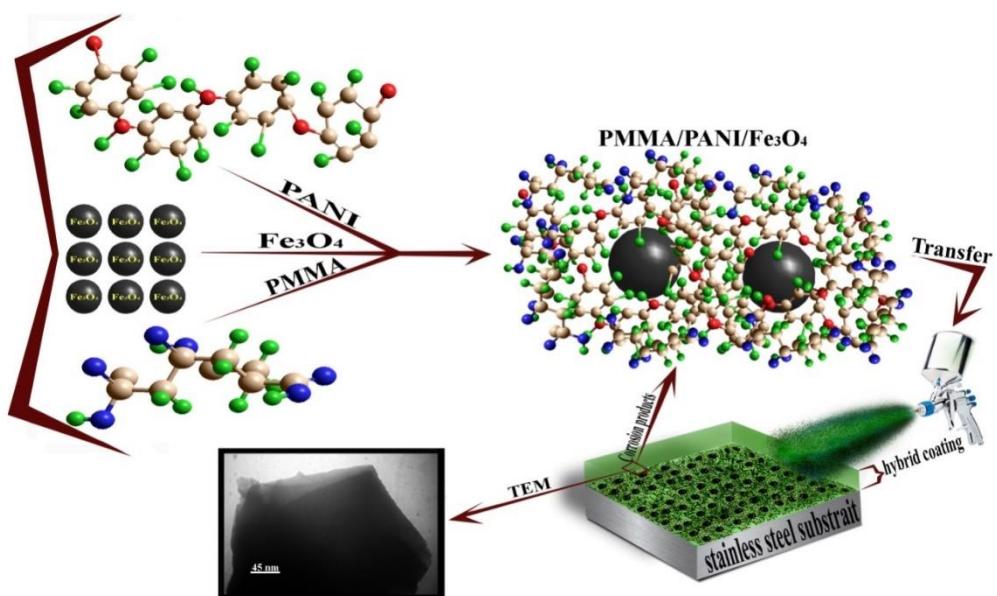
In order to synthesize PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites, a certain amount of PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites were slowly introduced into PMMA solution, and then the resulting suspension was stirred at a stirring rate of 500 rpm at room temperature

for 24 h. The resulting composites were then used as coating agent.

### 2.3. Substrate Processing

In this work, in order to conduct corrosion inhibition tests, the specimens were used and they were made from mild steel working electrode with the following composition (wt%): C: 0.027; Si: 0.0027; Mn: 0.34; P: 0.009; S: 0.003; Cr: 0.008; Ni: 0.03; Cu: 0.007; Al: 0.068; Nb: 0.003, Ti: 0.003, V: 0.003 and Fe balance. Mild steel specimens with a dimension of 20×20×1 mm, and 50×50×1 mm were used as substrates for the displacement of coating in electrochemical measurements. At first, all samples were treated by sanding after a disc polishing process, and subsequently were subjected to ultrasonic cleaning in an acetone solution for about 10 min. Next, they were rinsed with distilled water,

following which they were washed with ethanol for a period of 10 min. They, in the next step, were activated using 50 vol.% HCl solution for 2 min, and then were dried at room temperature. Eventually, to make a comparison, the PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating was used in the following two forms: (1) the pure form and (2) in combination with industrial paints at different concentrations (3, 6, 9, 12 wt. %). The nanocomposite coating was placed on the mild steel plates with a 12 mm diameter roller, and stored on a surface for 24 h to be dried at room temperature. A 3.5 wt% NaCl solution was obtained by dilution of analytical grade NaCl with double distilled water. The entire experiment was conducted in untouched solution at about 23 °C .



**Figure 1.** The schematic diagram of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating preparation.

### 2.4. Electrochemical Corrosion Evaluation

Corrosion experiments were performed in a three-electrode system which consisted of mild steel sheet (as working electrode), Pt wire (as auxiliary electrode), and Ag/AgCl (3 M KCl) (as reference electrode). Tafel polarization and EIS were employed to measure the resistance of coating against

corrosion in 3.5% NaCl solution. Prior to polarization tests, substrates were immersed in the above solution, and then the open circuit potential (OCP) was carefully observed to reach a fixed amount of potential. Potentiostat polarization and OCP were recorded through the use of PGSTAT204 equipment (MetrohmAutolab B.V., Netherlands). The potential of

potentiodynamic polarization was removed at a scan rate of 10 mVs<sup>-1</sup>, in a potential limit of  $\pm 250$  mV vs. OCP. To recognize the Tafel corrosion potential, two curves of anodic and cathodic polarization were obtained and then the regions were extrapolated to the corrosion potential ( $E_{corr}$ ) to obtain corrosion current density ( $I_{corr}$ ).

EIS was carried out using a frequency response detector (EG&G model 1025) with an electrochemical setup controlled by M 398 software. The range of frequencies to obtain EIS results were between 0.01 and 100,000 Hz. It should be noted that EIS tests were conducted at OCP. To evaluate the impedance spectra, the resulting experimental data was fitted into equivalent circuits with Zview software.

## 2.5. Microstructural and Electrochemical Characterization

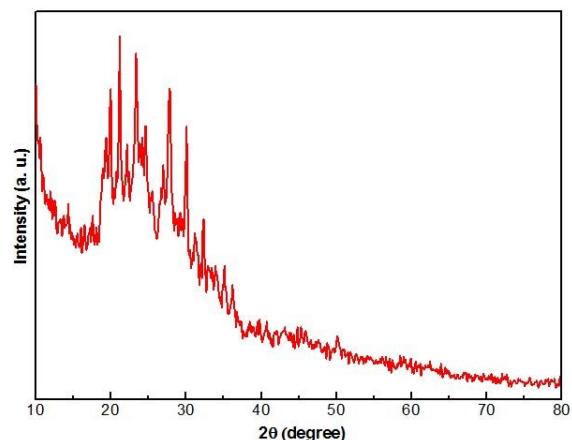
The crystalline structure of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating was studied by means of XRD analysis. The diffraction patterns of the PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> was obtained with PHILIPS Diffractometer (D5000). The data were collected within  $2\Theta$  angle from 10° to 80° using Cu K $\alpha$  line ( $\lambda = 0.15418$  nm). The functional groups and structure of the PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nano-composite coating was determined by FT-IR. Infrared spectra in the range 400–4000 cm<sup>-1</sup> on the sample pellets made with KBr were measured by using Bruker Tensor 27 spectrometer. SEM (Ziess MV2300) and TEM (Ziess 80 kV) analyses were adopted to characterize the morphologies of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating through the use of an LEO 1455 UP analyzer (Ziess MV2300). An AUTOLAB model PGSTAT30 was employed to run corrosion inhibition electrochemical tests of the PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nano-composite coating containing EIS and Tafel polarization. EIS studies were performed at corrosion potentials ( $E_{corr}$ ) over a frequency range of 10 kHz-0.1 Hz with a signal amplitude perturbation of 0.5 mV. Then

impedance data were analyzed through a Pentium IV computer and FRA software. A scan rate of 0.5 mV s<sup>-1</sup> was set during the Tafel polarization. The obtaining data were investigated by the GPES electrochemical software [23].

## 3. RESULT AND DISCUSSIONS

### 3.1. Characterization of Synthesized Nanocomposites

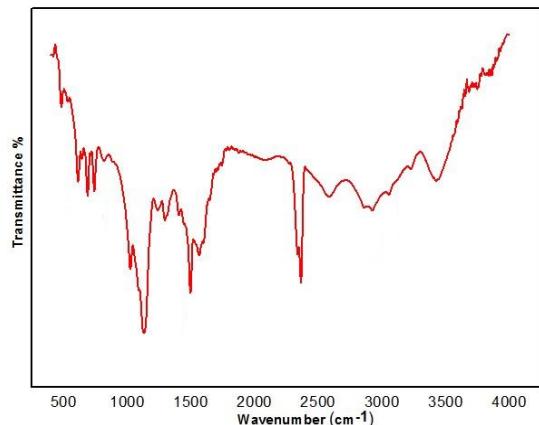
XRD spectra of the synthesized nanocomposite coating are shown in Figure 2. Looking at this figure, the strong Bragg peaks of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> revealed at angles of  $2\Theta \approx 22^\circ$  to  $31^\circ$  in the spectrum. These peaks demonstrate that the crystalline structure of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites was obtained, showing the regular arrangement of copolymer chains by chain-folding. Furthermore, this pattern indicates the structure of PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites were not changed during the preparation process [24, 25].



**Figure 2.** XRD diffraction patterns of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating.

FTIR pattern was used to characterize PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating. Therefore, FTIR pattern of the synthesized nanocomposites was plotted in the range of 400-4000 cm<sup>-1</sup>, presented in Figure 3. In this figure, the adsorption peak located at 592 cm<sup>-1</sup> was the characteristic peak of Fe–O bond which proving the presence of Fe<sub>3</sub>O<sub>4</sub> nanoparticles in the synthesized nanocomposites. Regarding PANI characteristic peaks, the peak

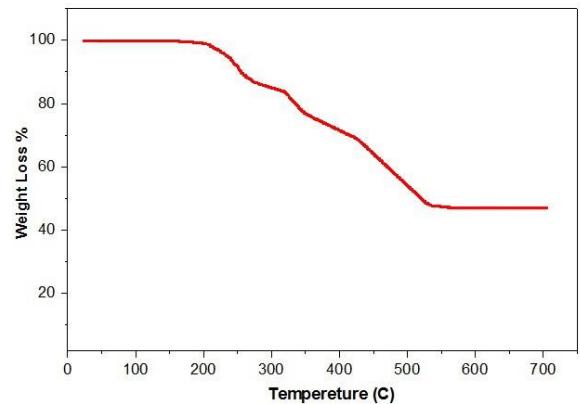
observed at around  $3500\text{ cm}^{-1}$  was assigned to the N–H stretching. In addition, the adsorption bonds located at approximately  $1500\text{ cm}^{-1}$  were ascribed to quinine ring and benzene ring of PANI. The presence of –CH<sub>3</sub>-substituted and C–N stretching adsorption groups in PANI structure were detected via the peaks occurred at  $1296\text{ cm}^{-1}$  and  $1301\text{ cm}^{-1}$ . The sharp peak observed at  $1633\text{ cm}^{-1}$  was assigned to C=O groups of PMMA. Furthermore, the bands in the  $2800\text{--}3000\text{cm}^{-1}$  region were from the stretching of C–H bonds of the saturated alkane existing in PMMA structure, confirming the presence of PMMA. According to these observations, PMMA resin and PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites were shown to be present in the synthesized nanocomposites [26–28].



**Figure 3.** The FTIR spectra of MMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating.

The thermal stability of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites was investigated via TGA analyses. To establish a balance, nitrogen was employed as the purge gas. Data were collected from the ambient temperature to  $700^\circ\text{C}$  at a rate of  $10\text{ }^\circ\text{C min}^{-1}$ . Moreover, the curve of the weight loss percentage versus temperature were plotted. In Figure 4, the TGA plot of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> in the atmospheric condition shows that 59.61wt% of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating was entirely decomposed at high temperatures (higher than  $500^\circ\text{C}$ ). The first signs of

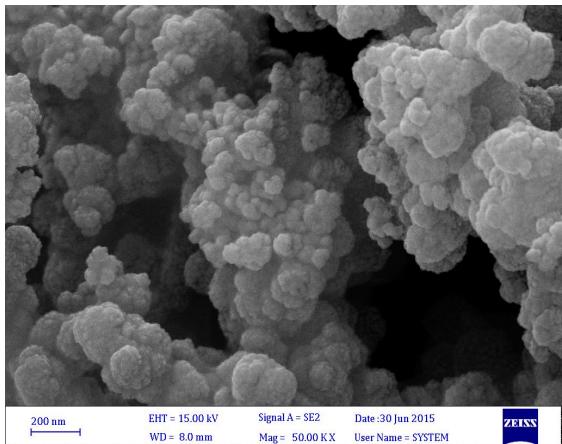
thermal transition were observed at  $125\text{--}275^\circ\text{C}$ , where the first weight loss at a lower temperature is primarily because of the elimination of moisture (up to  $125^\circ\text{C}$ ) and dopant anions ( $275^\circ\text{C}$ ). In addition, the main thermal decomposition for PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite composites coating occurred around  $300$  and  $500^\circ\text{C}$ . The degradation of this nanocomposite coating might occur due to the weak head-to-head bonding, solvent and impurities in the nanocomposites [29, 30].



**Figure 4.** TGA curve of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating.

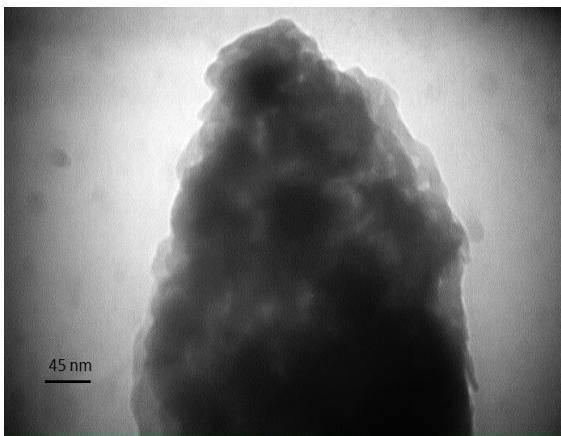
The surface morphology of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating was identified by means of TEM and SEM analyses. Figure 5, SEM image, depicts that PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating had a smooth surface with somehow spherical structure. Moreover, this image illustrates that the PANI and Fe<sub>3</sub>O<sub>4</sub> were evenly dispersed in the PMMA acrylic resin. That is to say, Fe<sub>3</sub>O<sub>4</sub> nanoparticles were strongly adhered to the polymeric networks formed by PANI and PMMA.

TEM image of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating is shown in Figure 6. Overall, as stated above, TEM image confirms the formation of a core-shell structure. As can be seen in the Figure 6, a pale-colored layers of PANI and PMMA were coated on the dark core of Fe<sub>3</sub>O<sub>4</sub> magnetic nanoparticle, with a thin coating layer of about 20 nm.



**Figure 5.** SEM image of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating.

Moreover, this image confirms that PMMA completely covered PANI/Fe<sub>3</sub>O<sub>4</sub> and the average size of the PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating microspheres was about 30 nm.



**Figure 6.** TEM analysis of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating.

### 3.2. Potentiodynamic Polarization Studies

The corrosion resistance of the coating was evaluated through cyclic potentiodynamic polarization measurements. Figure 7 presents the typical potentiodynamic polarization curves achieved from the industrial alkyd paint without coating and modified alkyd paint with different contents of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> coated mild steel substrates in a 3.5% NaCl solution. The values of  $b_a$  and  $b_c$  (Tafel slopes),  $E_{corr}$

(corrosion potential),  $I_{corr}$  (corrosion current),  $R_p$  (polarization resistance) obtained from extrapolation of Tafel plot and  $\eta_p$  (protection efficiency) are listed in Table 1. The equation below was used to obtain the protection efficiency of coating:

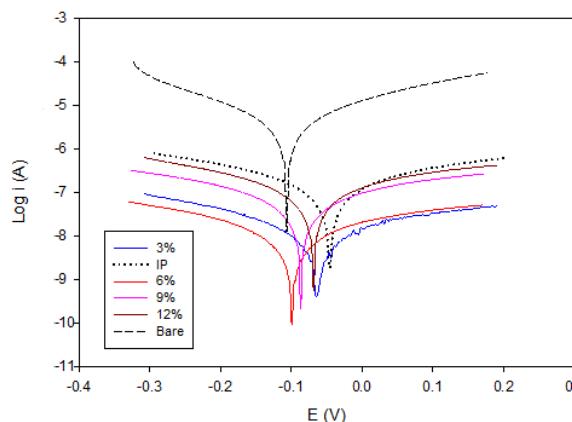
$$\eta_p = \frac{I_{corr} - I_{corr(c)}}{I_{corr}} \quad (1)$$

where  $I_{corr}$  and  $I_{corr(c)}$  are the corrosion currents in the absence and the presence of a coating, respectively.

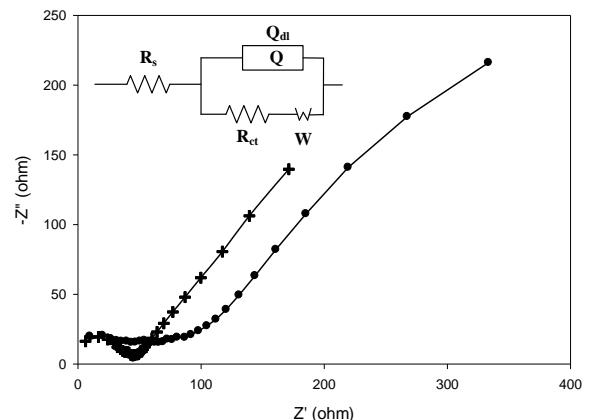
Obtained results revealed that the corrosion potential of coated samples shifted towards more positive values. This positive change of  $E_{corr}$  was an indication of anodic protection of the mild steel surface by the implemented coatings. According to the Tafel plots in Figure 7, a significant reduction in both cathodic and anodic currents was observed when mild steel was coated with the modified alkyd paint. These types of coating curbed the anodic and cathodic reactions of mild steel in an aggressive medium, so that the  $I_{corr}$  values declined from  $5.82 \times 10^{-6} \text{ A/cm}^2$  for bare mild steel to  $1.80 \times 10^{-8} \text{ A/cm}^2$  for 6% PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> sample, resulted in a desirable  $\eta_p$  of above 99%. These findings indicate that  $I_{corr}$  was considerably dependent on the nanocomposite percentage; that is to say 6% nanocomposite generated the lowest  $I_{corr}$ , while  $I_{corr}$  for samples containing 9 and 12% nanocomposites were much higher ( $8.03 \times 10^{-8}$  and  $1.64 \times 10^{-7}$ , respectively). Such observations could be due to the different conductivity and porosity properties of coating used. It can be stated that in the case of 6% PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> coating, nanocomposites were uniformly dispersed on the surface of the substrate mild steel, in comparison with the samples with higher compositions. This means that the proper dispersion, without agglomeration, led to a better conductivity in the resulting coating layer and that is why the corresponding  $I_{corr}$  and  $\eta_p$  were the most desirable among other samples.

**Table 1.** Corrosion parameter obtained from Tafel plots for bare mild steel, industrial paint, and different composition PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite modified paint.

Sample	b <sub>a</sub> (V/dec)	b <sub>c</sub> (V/dec)	E <sub>corr</sub> (V)	I <sub>corr</sub> (A/cm <sup>2</sup> )	R <sub>P</sub> (Ω)	η <sub>p</sub>
Bare Steel	0.26342	0.18093	-0.10624	5.82×10 <sup>-6</sup>	10190	-
IP	0.42403	0.34367	-0.045585	2.07×10 <sup>-7</sup>	508140	0.96443
IP+NP (3%)	0.52771	0.26261	-0.062624	1.89×10 <sup>-8</sup>	5.13×10 <sup>6</sup>	0.99675
IP+NP (6%)	0.48796	0.33243	-0.099016	1.80×10 <sup>-8</sup>	6.07×10 <sup>6</sup>	0.99691
IP+NP (9%)	0.40299	0.30309	-0.086641	8.03×10 <sup>-8</sup>	1.19×10 <sup>6</sup>	0.98620
IP+NP (12%)	0.52983	0.3142	-0.068774	1.64×10 <sup>-7</sup>	665890	0.97182



**Figure 7.** Tafel plots for bare mild steel, industrial paint, and different composition PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite modified paint.



**Figure 8.** Nyquist plots of (+) industrial paint and (●) Pure PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coated mild steel in 3.5% NaCl solution.

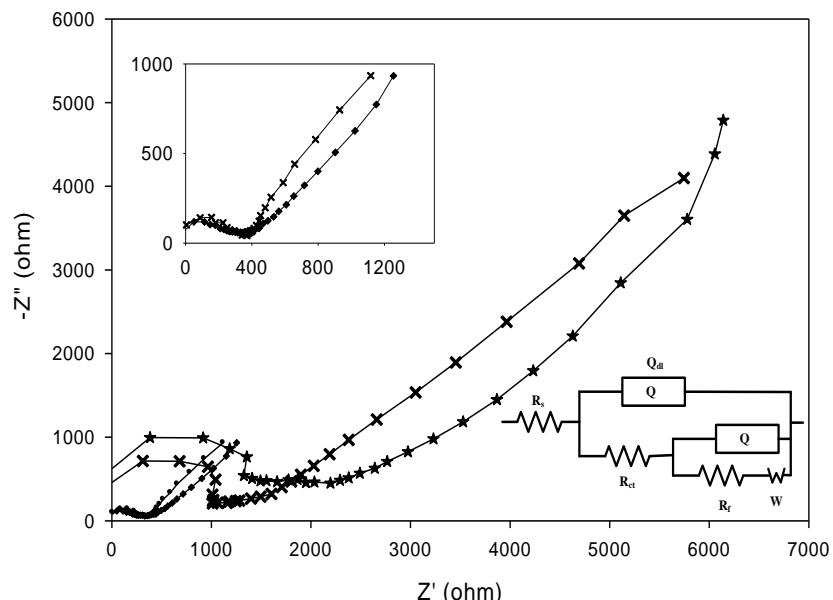
Figure 8 illustrate Nyquist plots of industrial paint and pure PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating. In addition, obtained Nyquist plots of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating with various compositions in 3.5% NaCl solution are depicted in Figure 9. Impedance data for samples were fitted with equivalent circuit models and are indicated in the insets of Figure 8 and Figure 9. In the equivalent circuits models, R<sub>s</sub> stands for the resistance of the solution, R<sub>ct</sub> indicates the charge transfer resistance at high frequencies, R<sub>f</sub> shows the film resistance of the adsorption of inhibitor molecules and all other accumulated species at metal-solution interface in the low-frequency region, Q<sub>dl</sub> and Q<sub>f</sub> are the constant phase elements (CPE), representing double-layer capacitance and film capacitance,

respectively, and W is the Warburg impedance [31].

The values related to the representative parameters of the optimal fit to the obtained data by the two circuit models are summarized in Table 2. According to Table 2, the R<sub>ct</sub> value increased from 38.3 Ωcm<sup>2</sup> for the industrial paint to 76.04, 329.8, 1027, 1685 and 280.6 Ωcm<sup>2</sup> for the pure nanocomposite and 3, 6, 9 and 12% nanocomposite coated samples, respectively. A consistent and flawlessly coated metallic surface can be identified by higher R<sub>ct</sub> and R<sub>f</sub> and lower Q<sub>dl</sub> and Q<sub>f</sub> [32]. The higher R<sub>ct</sub> and R<sub>f</sub>, and the lower Q<sub>dl</sub> and Q<sub>f</sub> for nanocomposite-modified paint indicated that the presence of the nanocomposites with 6-9% composition resulted an excellent corrosion performance for mild steel.

**Table 2.** The EIS parameters of industrial paint and different composition PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite modified paint.

Sample	R <sub>s</sub> (Ωcm <sup>2</sup> )	Q (Fcm <sup>-2</sup> )	N	R <sub>f</sub> (Ωcm <sup>2</sup> )	Q (Fcm <sup>-2</sup> )	n	R <sub>ct</sub> (Ωcm <sup>2</sup> )	W (Ωcm <sup>2</sup> )
IP	4.2	-	-	-	4.32×10 <sup>-7</sup>	0.878	38.3	1.98×10 <sup>-2</sup>
NP	9.7	-	-	-	3.74×10 <sup>-5</sup>	0.524	76.04	1.06×10 <sup>-2</sup>
IP+NP (3%)	20.04	3.20×10 <sup>-8</sup>	0.82	60.88	2.90×10 <sup>-3</sup>	0.48	329.8	6.24×10 <sup>-4</sup>
IP+NP (6%)	21.59	3.57×10 <sup>-9</sup>	0.9	57.11	4.04×10 <sup>-4</sup>	0.49	1027	4.57×10 <sup>-4</sup>
IP+NP (9%)	16.15	2.74×10 <sup>-9</sup>	0.88	50.02	3.1×10 <sup>-4</sup>	0.43	1685	2.89×10 <sup>-4</sup>
IP+NP (12%)	15.85	2.1×10 <sup>-8</sup>	0.86	35.4	1.46×10 <sup>-4</sup>	0.48	280.6	2.52×10 <sup>-4</sup>



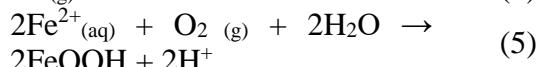
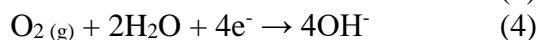
**Figure 9.** Nyquist plots of different compositions of PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite modified paint in 3.5% NaCl solution, (●) 3% nanocomposite, (×) 6% nanocomposite, (★) 9% nanocomposite, (◆) 12% nanocomposite.

Table 3 represents a comparison of corrosion resistance of various polyaniline coatings. Compared with other works, according to the Icorr, Ecorr and the anticorrosion efficiency, prepared coating in this work has a good barrier effect on corrosion of mild steel.

### 3.3. Anticorrosion Mechanism

It is generally accepted that the steel corrosion process includes reduction and

oxidation reaction which are summarize as below [33]:



As it is obvious, the corrosion process of mild steel is considerably related to the presence of enough O<sub>2</sub> and H<sub>2</sub>O. To halt or

slow down one of these reactions would be effective when it comes to protecting the substrate mild steel from rust formation. For that reason, a desirable coating agent should

effectively be capable of retarding these reactions, which generally done via physical or electrochemical protection [34].

**Table 3.** A summary of studies about PANI nanocomposites in enhancing the corrosion resistance of coatings.

Materials	Substrate	Icorr ( $\mu\text{A cm}^{-2}$ )	Ecorr (mV)	Efficiency (%)	Reference
polyaniline-SiO <sub>2</sub>	mild steel	0.09	-	99.93	[35]
polyaniline/graphene	mild steel	0.38	-537	53.49	[36]
Polyaniline-clay- epoxy	mild steel	0.061	-664	76.20	[37]
PANI-Fe <sub>2</sub> O <sub>3</sub> - alkyd resin	mild steel	1.8	-962	-	[38]
Polyaniline-Boron nitride-PVA	mild steel	1.03	-44	90.95	[39]
This work	mild steel	0.018	-99	99.69	

As a superb coating material, PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites protected the surface of mild steel via the formation of an impermeable layer upon its surface, referred to as physical protection. This means that the protecting layer served a crucial role in inhibiting the diffusion of corrosive agents, such as O<sub>2</sub> and electrolyte molecules, to the surface of mild steel through the formation of a physical barrier. Furthermore, in terms of electrochemical protection, the existing PANI/PMMA in the nanocomposite coating structure might take part in electrochemical corrosion reactions, retarding the corrosion of underlying steel. In other words, it was PANI/PMMA molecules that constantly reduced and oxidized in cyclic electrochemical reactions instead of the substrate mild steel layer, as a result of which the substrate was intact and protected against corrosion reactions.

#### 4. CONCLUSION

In this paper, the anti-corrosion ability of modified industrial alkyd paint with PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites on mild steel was studied. The corrosion behavior of coated mild steel was evaluated

via potentiodynamic polarization and EIS techniques, both conducted in 3.5% NaCl solutions. Firstly, PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites were synthesized. Through characterization procedures, namely XRD, FTIR, SEM, TEM and TGA, the nanocomposites were elementally, morphologically and thermally analyzed. Afterward, the modifying effects of the synthesized nanocomposites were studied by means of Tafel polarization and EIS methods, in which the nanocomposites were blended with industrial alkyd paint. Based on these methods, 6% PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposite coating produced significant protection against corrosion; with I<sub>corr</sub> of  $1.80 \times 10^{-8} \text{ A/cm}^2$  and η<sub>p</sub> of more than 99%. As a result, PMMA/PANI/Fe<sub>3</sub>O<sub>4</sub> nanocomposites could be recommended as a promising coating material, and one will achieve desirable corrosion results when blending these with industrial alkyd paint, particularly, for mild steel protecting purposes.

#### CONFLICT OF INTEREST

The authors declare that they have no conflict of interest.

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