Influence of Adding SiC on Microstructure and Electrical Properties of ZnO-based Nanocomposite Varistor

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Abstract:

In this research the influence of adding SiC on microstructure and electrical properties of ZnO-based Nanocomposite varistors were investigated. SiC was added with amounts of 10-0 mass% to ZnO-based varistor composition. It is found that SiC allows reaching to high threshold voltage with formation of fine-grained ZnO. Another important effect of adding SiC is formation Zn_2SiO_4 (Willemite) on the surface of SiC grains. With this effects SiC had great influence on Varistor electrical properties. On the other hand relative density decreased with increasing percentage of SiC in the composition. Hence with adding SiC to the composition, the threshold voltage of varistors (VT) and non-linear coefficient (α) increased at first and then decreased with increaseing of porosity. Also Current leakage decreased at first and then increased with adding more SiC. Also ZnO powder size effect on the final properties was examined in this reasearch by using submicron size and Nano size ZnO powder. The best achieved electrical result was threshold voltage as large as 4220 V/cm and non-linear coefficient α and ZnO powder and adding %4 SiC to the composition. **Keywords:** Electrical properties, Grain growth, Nanocomposite, SiC, Varistor, ZnO.

1. INTRODUCTION

Varistors (variable resistors) are voltage-dependent resistors with a symmetrical V/I characteristic curve whose resistance decreases with the increase of voltage. The voltage dependence of varistors or VDRs (voltage dependent resistors) may be approximately characterized by the formula

 $I = KV^{\alpha} \tag{1}$

Where K is constant and α denotes the non-linearity exponent and in this way may be interpreted as a measure of the steepness of the V/I characteristic [1-2].

The first known ceramic material showing that property is the silicon carbide (SiC). This ceramic

material consists of SiC particles (ranging from 50 to 100 μ m in size), intimately bonded to a silica rich vitreous matrix.

Single phase BeO doped SiC varistors was developed by hot isostatic pressing. Despite having superior electrical resistance than multiphase SiC varistors, the ceramic's non-linear coefficient remained low (α =5).

On the other hand high non-linear varistor materials (α =50) were developed by Matsuoka. Those ceramics have complex chemical composition constituted by ZnO as major component, and small amounts of Bi₂O₃, Sb₂O₃, CoO, MnO₂ and Cr₂O₃. Their microstructure is multiphase being formed by ZnO grains as predominant phase and many

	C		mass %					
	Compositi	on ZnO	SiC	Bi ₂ O ₃	Sb_2O_3	CoO	PVA	
	А	95	0	3	1.5	0.5	0.75	
	В	93	2	3	1.5	0.5	0.75	
	С	91	4	3	1.5	0.5	0.75	
	D	89	6	3	1.5	0.5	0.75	
	Е	87	8	3	1.5	0.5	0.75	
_	F	85	10	3	1.5	0.5	0.75	
perature (C°)	1200	1100 C 60 min						
	1000							
	800			5 C°/min			700 0	
	600		2 C°/min				✓ /00 C	
	400	5 C°/min						
E a	200 2	C°/min						
Ĕ	0 🖊 🗂	C°/min						
	0	50	100	150 2	00 250	300	350	
	Time (minute)							

Table 1: Chemical composition of samples

Figure 1: Rate of heating varistor samples

other phases like the spinel $(Zn_7Sb_2O_{12})$, pyrochlore $(Zn_2Bi_3Sb_3O_{14})$ and several polymorphic phases of bismuth oxide, distributed in the structure [3].

ZnO based varistors exhibit highly non-linear current–voltage characteristics which find application in the field of protection gainst transient voltage surges. In doped ZnO ceramics non-linearity coefficients as high as α =70 can be achieved. In standby, the varistor is subjected to a voltage below its characteristic breakdown voltage and only a leakage current pass through the bulk specimen. During transient surge the voltage between electrodes exceeds the breakdown voltage and the varistor becomes highly conductive diverting the current to ground and so protecting the circuit.

The non-linear response originates on its polycrystalline microstructure and more specifically on detailed processes occurring at the grain/grain interfaces. By proper doping, the near grain boundary region becomes highly resistive while the grain interior turns into conductive, and electrostatic potential barriers build up at the grain boundaries due to charges being trapped at interface states [4]. In fact in Ceramic varistors based on the ZnO– Bi_2O_3 -Sb₂O₃ system the characteristic non-linear current-voltage response is a consequence of their microstructure and electronic structure. Non-ohmic behavior is due to the presence of electrically active grain boundaries, formed by an intergranular Bi_2O_3 -rich phase that separates the semiconducting ZnO grains. Besides Bi_2O_3 , other oxides enter in minor proportions into the varistor composition (Sb₂O₃, CoO, MnO₂ and Cr₂O₃). Their role is to improve the electrical response [5].

With consideration that ZnO based varistors and SiC based varistors are used as two important generation of varistors, it seems that there is a vacant place in research papers to examine the properties of ZnO-SiC composite as a varistor. We know that SiC has a very strong covalent bond. As a tough material SiC can prevent the ZnO grain growth and help to have tinier microstructure. In the present work, influence of amount of added SiC and also affection of using Nano size ZnO powder on microstructure, final density, and current–voltage (I–V) characteristics of ZnObased varistor ceramics has been investigated.

2. EXPERIMENTAL

The basic formulation and preparing process in current research were chosen like conventional varistor formula and process. Analytical grades of ZnO (Zinchem, 300-900 nm), ZnO (Nano Amor, 20 nm), SiC-β (Nano Amor, 45-55 nm), Bi₂O₂ (Nano Amor, 90-210 nm), Sb₂O₂ (Nano Amor, 90-210 nm), CoO (Nano Amor, 90-210 nm), and PVA (Sigma), were used in this work. SiC- β was chosen because mobility of SiC- β is higher than SiC- α and thus the electrical resistance of SiC- β is lower than SiC- α [6]. In this paper the samples which made by Nano size ZnO powder are called Nano samples and the samples which made by Submicron size ZnO powder are called Submicron samples. The composition of the samples are shown in Table 1.

2.1. Sample preparation

The samples were prepared by conventional method. Table 1 shows the chemical compositions of samples prepared in this research. The oxide powders were weighed and then mixed during 20 min with Alumina balls and distilled water in fast mill. The Aqueous slurry obtained was dried in 80°C during 24 h. Then dry milling of the dried batches was carried out during 20 min in fast mill without water just by alumina balls. The batches were molded in discs of 20 mm diameter and 3 mm in thickness under pressure of 100 Mpa by using hydraulic isostatic press. Then the green bodies were sintered at 1100°C for 1 h. The maximum sintering temperature was chosen based on other researcher experiences [7-8].

The rate of heating is shown in Figure 1. It was chosen with considering some physical and chemical reactions during the heating. Some of the important chemical reactions are as below [1, 9-10].

2.2. Density measurment and Analyzing of microstructure and phases

The density of the pellets was measured by Archimedes method.

$$\rho = W_d / W_w - W_s \tag{7}$$

$$\% RD = (\rho / \rho_{tb}) \times 100$$
(8)

Where ρ is density, Wd is dry weight, Ww is wet weight, Ws is soaking weight, oth is theoretical density that were measured for each composition, and %RD is relative density. To observe the microstructure scanning electron microscope (SEM, TESCAN-VEGII XMU, Czech) was utilized. In order to remove ZnO from surface and emerge grain boundaries, the pellets were polished and etched with 5 molar NaOH solution. Also the samples were coated with gold to be ready for SEM analyzing. The crystalline phases were identified by an X-ray diffractometer (STADI-MP, Germany) using 40 KV voltage and 30 mA amperage and Cu Kα as a radiation source.

2.3. Measurement of V–I characteristics

For electrical varistor test, the pellets were polished and coated by conductive Carbon onto both faces with using conductive Carbon spray (KONTAKT CHEMIE, Belgium). For avoiding of surface current effect, the bodies were coated on the side part by an insulator epoxy resin. The I-V characteristics were measured at low currents until 10 mA under continuous voltage. The voltage-current (V-I) characteristics were measured by using a V-I source/measure unit. The nominal varistor voltages (V_{y}) (breakdown voltage is the voltage at which the varistor switches from a highly resistive to a highly conductive state) at 1 and 10 mA and the threshold voltage V_T (V/mm) (breakdown voltage/

$$Sb_2O_3 (s) + O_2 (527^{\circ}C) \rightarrow Sb_2O_5 (l)$$
 (2)

$$Sb_2O_5(l) + ZnO(s)(700-800^{\circ}C) \rightarrow ZnSb_2O_6(s)$$
(3)

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$$ZnSb_2O_6(s) + 6ZnO(s) \approx 2n_7Sb_2O_{12}(s)$$

$$\tag{4}$$

$$2Zn_2Bi_3Sb_3O_{14} + 17ZnO (950-1050°C) \rightarrow 3Zn_7Sb_2O_{12} + 3Bi_2O_3$$
(5)

$$3ZnSb_2O_6 (s) + 3Bi_2O_3 (s) + ZnO (s)(900-700^{\circ}C) \rightarrow Zn_2Bi_3Sb_3O_{14}(s)$$
 (6)

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unit thickness of varistor ceramic) were measured. $V_T = V_N (1mA)/d$, where d is the thickness of the sample in mm) and the non-linear coefficient α $(\alpha = \log(I_{10mA}/I_{1mA})/\log(V_{10mA}/V_{1mA}) = 1/\log (V_{10mA}/V_{1mA})$ according to the equation describing the V–I non-linearity of the varistor ceramics I = KV^{α}) were determined. The leakage current (I_L) (the current through the varistor in the pre-breakdown region of the V–I characteristic) was measured at 0.75 V_N (1mA) [7].

3. RESULTS AND DISCUSSION

Six different varistor samples with different compositions were constructed. Figure 2 shows SEM micrographs of ceramic varistors sintered 1 h in 1100°C with 0, 2, and 6 mass% of SiC content. As can be seen, basically, the growth of ZnO grains was prevented by SiC grains and therefore the average of ZnO grain sizes decreased as the amount of SiC increased. From the other point of view, densification has been limited by increasing the amount of SiC. With the increase of mass% of SiC from 0% up to 10 % in the composition, the average of ZnO grain size decreased from 4 μ m to 2 μ m and the amount of porosity increased from 6% up to 25%.

So it will have two different effects on the varistor properties: 1-decreasing ZnO grain size 2increasing the amount of porosity. For investigation of ZnO initial powder size effects on the final microstructure of varistors, series of samples were prepared with using ZnO nano size powder with the same formula. As can be seen in Figure 2 the average of ZnO grains in the samples content nano ZnO didn't have sensible difference to the samples which prepared by submicron size ZnO.

The increasing of porosity with adding SiC was verified by measuring density. The density of samples was measured by Archimedes method. The results are shown in Figure 3. It can be realized a sensible decrease in density of samples from 94% to 73% with the increasing amount of SiC from 0% to 10% in the composition. This event might be occurred by two reasons. Firstly SiC seeds as a physical barrier can prevent the ZnO grains to reach each other during the sintering. Hence SiC prevents densification process. Secondly vaporization of Carbon due to oxidation of SiC in high temperature can make porosities in the microstructure of samples. A similar rate of decreasing in density was occurred in nano samples. But nano samples revealed a higher density in comparison to submicron samples. In nano samples the average of relative density was about 2% higher than Submicron samples.



Figure 2: SEM image of varistor samples with different composition: (a) 0% SiC with submicron ZnO; (b) 2% SiC with submicron ZnO; (c) 6% SiC with submicron ZnO; (d) 0% SiC with nano size ZnO; (e) 2% SiC with nano ZnO



Figure 3: Relative density of sintered samples using Sub Micron ZnO and Nano ZnO



Figure 4: XRD pattern of varistors with different composition (*W*: Willemite, *P*:Pyrochlore, *Z*:*ZnO*, *S*:*Spinel*, *SiC*: *Silicon carbide*): (*a*) 0% *SiC*; (*b*) 4% *SiC*

Several phases were identified by assisting EDX and XRD analyses. XRD patterns of the investigated samples are given in Figure 4.

According to XRD peaks in the sample without SiC, three phases were identified: ZnO phase as the main phase, $Zn_7Sb_2O_{12}$ -type Spinel phase, $Zn_2Bi_3Sb_3O_{14}$ Pyrochlore phase. In samples which had SiC content ,moreover the mentioned phases, additional peaks were evident and their intensity

increased with the increasing of SiC amount in the starting composition .These phases were identified as be SiC- β ,and Willemite (Zn₂SiO₄). Willemite is created by combination ZnO and the layer of SiO₂ on the surface of SiC grains. Due to this fact that the SiC- β 's peaks were existed in XRD patterns, so it can be say that there is possibility of existing of remained SiC- β in the core of Willemite phase.

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The likely position of willemite, SiC, and ZnO phases is shown in Figure 5. I-V electrical test of samples was carried out. Characteristic curves of varistor samples with six different amounts of SiC and two different ZnO grain sizes are depicted in Figure 6. As can be seen, all the samples showed varistor electrical behavior. Also threshold voltage, α and current leakage of varistor samples were displayed in Figure 7. The leakage current (I_L) was measured at 0.75V_N (at 1 mA).



Figure 5: Schematic image of likely position of willemite, SiC, and ZnO phases in ZnO-SiC based varistor

All the charts had an optimum point. As can be seen the threshold voltage and α increased and then decreased, and the current leakage decreased and then increased as the amount of SiC increased in the composition. Regarding to the SEM micrographs the increasing of SiC amount in the composition will cause to decrease of final ZnO grain size. Referring to equation 1, threshold voltage will increase if the ZnO grain Size decreases. So raising of SiC amount in varistor composition will cause to reduction of ZnO grain size and hence it will result in the threshold voltage rise.

$$V_{\rm T} = 3d/D \tag{9}$$

Which V_T : Threshold voltage, d: Varistor thickness, D: Average of ZnO grain sizes. Also based on the final composition another likely reason for rising the threshold voltage with the increasing of SiC amount can be mentioned. With consideration of XRD patterns it can be realized that by adding SiC in the varistor composition, a new phase that name is Willemite is created. Based on this fact that



Figure 6: I-V curves of varistor samples: (a) with submicron ZnO; (b) with nano ZnO







Figure 7: Influence of adding SiC on threshold voltage, non-linear coefficient α , and current leakage of varistor: (a) with using submicron ZnO; (b) with using nano ZnO

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Willemite is a high electrical resistant phase with an electrical band gap as high as 5.5 ev [11], creation of this phase can cause to increase of threshold voltage.

On the other hand with continuance adding SiC, as it was shown in Figure 3 the density of samples decreased and it means the amount of porosity increased. So with continuance of adding SiC the amount of porosity increased and therefore the threshold voltage decreased. Also the non-linear coefficient α was affected by adding SiC and the Creation of Willemite on the surface of SiC grains is the most likely reason of the increasing α by adding SiC to the composition.

Willemite is created by combination ZnO and the layer of SiO₂ on the surface of SiC grains. So the final obtained microstructure will be a High resistant phase (Willemite) between to semi conductor grains (ZnO & SiC) which is ideal for having a varistor with high α . Morover the band gap of SiC is smaller in comparison to ZnO [12-13]. As like as threshold voltage, non linear coefficient α decreased with adding more SiC duo to increase of porosity. Also current leakage (I_L) is affected by SiC amount. I_L is the current which pass through the grain boundaries before threshold voltage.

With adding SiC, Willemite will be created in grain boundaries; and due to high electrical resistance of Willemite, current leakage decreases. With continuance of adding SiC, the amount of porosity will be increased and so it will cause to increase the current leakage. Regarding to the results the rate of the variation of electrical properties with SiC amount in Nano samples was lower than submicron samples. In addition, Nano samples were shown higher threshold voltage, higher α , and lower current leakage in comparison to submicron samples.

4- CONCLUSION

The influence of adding SiC to ZnO based varistor on electrical and physical properties of varistor was investigated in this research. Regarding to the results, adding SiC to ZnO based varistor samples, decreased the ZnO grain growth process. So the final structure of varistor was finer with using SiC in the composition and it influenced on electrical properties.

On the other hand there is another effect on varistor physical properties by adding SiC that is decreasing density. So these two different effects will cause to different electrical behaviors. At first threshold voltage and α increased by adding SiC and then decreased as the porosity increased. Also current leakage decreased at first and then increased.

The influence of ZnO grain size also was studied in this work. Using Nano ZnO didn't have sensible effect on final grain size but it improved the equality of microstructure and electrical properties. The best achieved electrical result was threshold voltage as large as 4220 V/cm and non-linear coefficient $\alpha = 44$ that were gained by using of Nano ZnO powder and adding 4% SiC to the composition.

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